

## **INVESTIGATION OF THE FRETTING PHENOMENON**

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Abstract: Fretting damage is often the origin catastrophic failures or loss of functionality in many industrial applications. Considered as a plague for modern industry, fretting is encountered in all quasi-static loadings submitted to vibration and thus concerns many industrial branches. The main parameters were reported to be amplitude displacement, normal load, frequency, surface roughness and morphology, and residual stresses. The present paper argues that adhesion forces and elastic deformation in the contact zone may contribute significantly to the relative displacement during fretting of metals.

### **1. INTRODUCTION**

Fretting is now fully identified as a small amplitude oscillatory motion which induces a harmonic tangential force between two surfaces in contact. It is related to three main loadings, i.e. fretting-wear, fretting-fatigue and fretting corrosion.

The main parameters were reported to be amplitude displacement, normal load, frequency, surface roughness and morphology, and residual stresses. More recently fretting has been discussed using the third-body concept and using the means of the velocity accommodation mechanisms introduced by Godet et al.[1,4]

Fretting regimes were first mapped by Vingsbo. In a similar way, three fretting regimes will be considered: stick regime, slip regime and mixed regime. The mixed regime was made up of initial gross slip followed by partial slip condition after a few hundred cycles. Obviously the partial slip transition develops the highest stress levels which can induce fatigue crack nucleation depending on the fatigue properties of the two contacting first bodies. Therefore prediction of the frontier between partial slip and gross slip is required.

The type of surface damage that occurs in fretting contact depends on the magnitude of the surface normal and tangential tractions. In existing fretting models the relative displacement is assumed to be accommodated mainly microslip in the contact surface.

The present paper argues that adhesion forces and elastic deformation in the contact zone may contribute significantly to the relative displacement during fretting of metals. A simultaneously applied tangential force and normal into contact appears a adhesion force. A tangential force whose magnitude is less equal on greater than the force of limiting friction will not give rise on give rise to a sliding motion. It is determined the energy loss dissipated per fretting cycle.

### **2. EXPERIMENTAL MEANS**

For the study of the fretting phenomenon in case of elastics assemblages spring slides with multiple sheets, I used the experimental stall from fig.1.[2,3]  
The stall permits testing for one slide and for spring slides with multiple sheets, too.

## 2.1. DESCRIPTION OF THE STALL

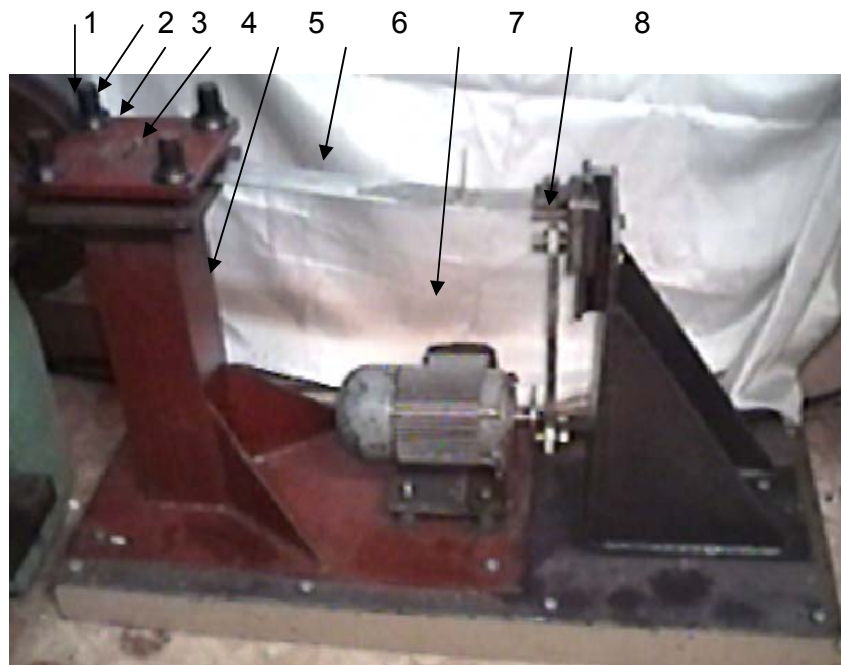
On the rigid support the elastic lamella (6) is assembling through the agency of the superior plate (4) and of the screws (1).

The assemblage is made through the agency of 8 balls (4 balls inferior and 4 superior balls) who assure a point contact between the ball and the lamella.

The elastic lamella (6) oscillates because of the rod crank mechanism with eccentric (8). This mechanism is actuated with the electrical engine assuring the necessary conditions for producing the fretting phenomenon.

The contact is charged with the assistance of 4 screws (1) through the agency of some helicoidally springs (2) and through the agency of some radial-axial bearings with conic rolls.

The helicoidally springs beforehand standard permit a charge with a normal and known force, the presence of the radial-axial bearings assuring the eliminate of friction between the screw and the superior plate.



**Fig.1. Experimental stall**

The stall can be used for the testing at fretting of some couples by different materials. This stall can be adapted for study of the lamellar springs with many sheets.

The lamellas used in experiments have the dimensions 560x56x2 mm and are realized by spring steel having hardness 55 HRC.

The balls are spring balls and have 19 mm in diameter. The lamella is supported in inferior side on 4 balls (fig.2) in superior side the charge of the contact is made through the agency of 4 balls. The rod-crank mechanism permits a displace at the end (extremity) of the 20 mm lamella and can modify this displace by changing of the system eccentricity (Fig.3). The system is actuated through the agency of electrical engine having revolution of 750 rot/min.

Helping with this experimental stall we can made fretting tries for normalize and different forces for different numbers of sollicitation cycles.

We obtained different wear traces corresponding fretting wear. So, we find the dependence of the normal charging force, and we can compare the different fretting traces by comparing of different fretting zones for certain conditions of contact.

Therewith we can compare the theoretical results previously presented with the experimental results. Traces wear obtained was assumed with a video camera and processing on the computer. The displacement at the contact level was determined, like we shown previously helping with the video camera and computer.

The determination of displacement was made for the two renges of balls.




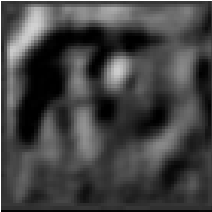
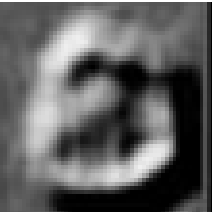
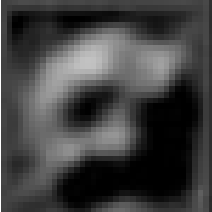

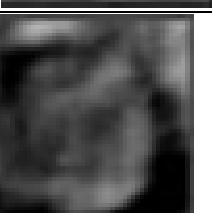
Fig.2 Inferior side



Fig.3. The system excentricity

In the table 1. are the traces wear obtained for a normal charcing of 200 N on the each screw.

Table 1

Number of cycles	Poziotion of balls	
	face	back
30000		
40000		
50000		

For comparing the traces wear obtained with the theoretical results obtained for the fretting phenomenon we determined the central area and the annular adjacent area, and the results are in the table 2 for the front balls and in the table 3, for the back balls.

In fig.4. and 5 are the dependence of the wear traces by the cycles numbers for a normal force by 200 N and for the two position of the balls in front and back.

Table 2

Nr. crt.	Loading [N]	Number of cycles	Area central [mm <sup>2</sup> ]	Radius central [mm]	Area ext. [mm <sup>2</sup> ]	Radius ext. [mm]	Area annular [mm <sup>2</sup> ]
1	200	30000	0.15300	0.22070	0.63278	0.4488	0.47978
2	200	40000	0.22219	0.26596	0.99215	0.5622	0.76996
3	200	50000	0.28807	0.30281	1.27996	0.6383	0.99189

Table 3

Nr. crt.	Loading [N]	Number of cycles	Area central [mm <sup>2</sup> ]	Radius central [mm]	Area ext. [mm <sup>2</sup> ]	Radius ext. [mm]	Area annular [mm <sup>2</sup> ]
1	200	30000	0.19752	0.25075	0.77363	0.4962	0.57611
2	200	40000	0.24173	0.27739	1.40647	0.6691	1.16474
3	200	50000	0.37215	0.34418	1.70178	0.7360	1.32963

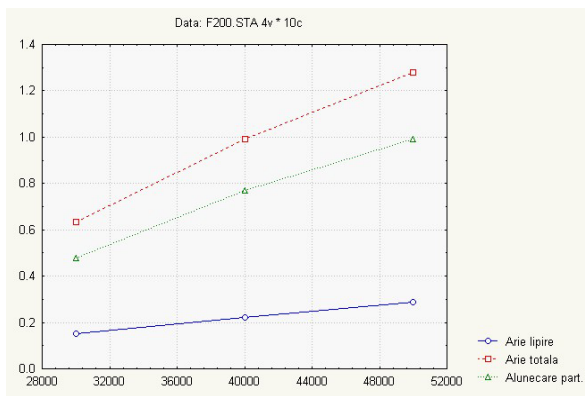


Fig.4. The dependence of the wear traces by the numbers of cycles for F= 200N; in front

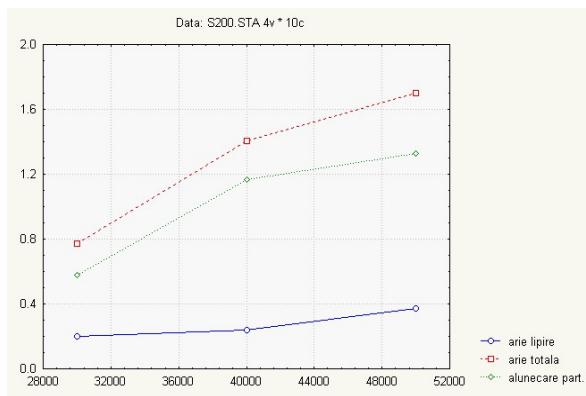


Fig.5. The dependence of the wear traces by the numbers of cycles for F= 200N;back

### 3.CONCLUSIONS

The experimental stall permits realization of the experimental tries for the study of fretting. We can determine the different size of the fretting areas and we can compare these with the theoretical results.

Can be made considerations for existence of one friction coefficient who is variable between the surfaces corresponding by one fretting contact.

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