

STRUCTURAL ANALYSIS AND SYNTHESIS OF PARALLEL MANIPULATORS

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The paper presents a new way of structural - topological analysis for parallel manipulators, with referring to the calculation of mobility (degree of freedom) of complex mechanisms. A parallel manipulator has a complex topological structure with joints (as kinematical pairs) of various types. For the parallel manipulators we present a new formula for mobility calculation related to the kinematical chain number, considered as identical legs. If we mark with  $N_l$  the number of kinematical chains, which are considered as legs for PMp, then the number of independent closed contours is  $N_l - 1$ . It is mentioned that the kinematical chain of a leg can be an open contour (fig. 1) or a complex contour with open and closed contours (fig. 2).

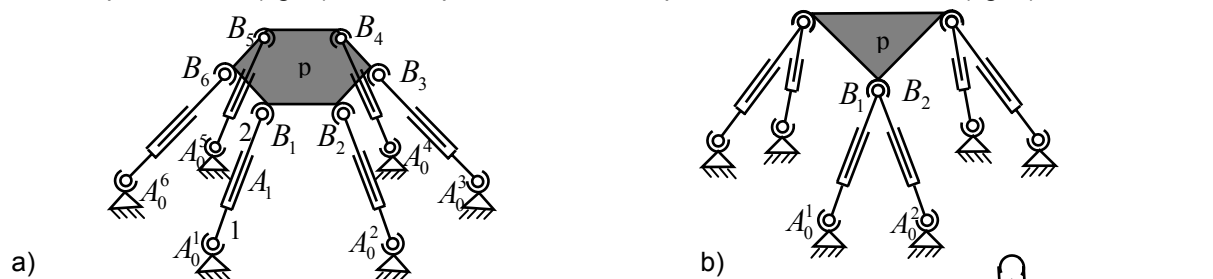


Fig. 1

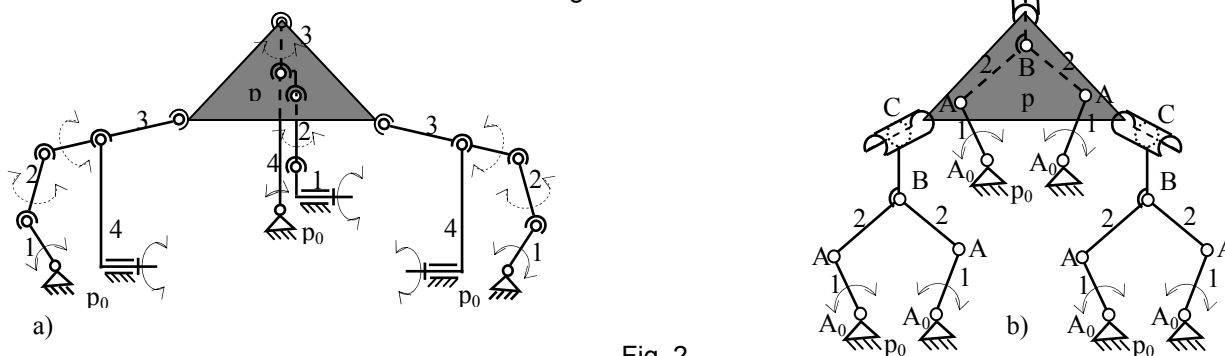


Fig. 2

The general formula of mobility for PMp-s from first category (fig. 1) is writes:  $M = (M_0 - r_c) \cdot N_l + r_c$ , where  $r_c$  is the rank of one closed kinematical contour with two legs. For example, for PMp (fig. 1), a leg is composed from two joints of class  $m=3$  and a joint of class  $m=2$ , therefore the mobility for them is  $M_0 = 2 \cdot 1 + 3 \cdot 2 = 8$ . The geometrical mobility of this PMp is calculated with previously formula, where  $r_c=6$  and  $N_l=6$ :  $M = (8 - 6) \cdot 6 + 6 = 18$ . The 18 DOF of PMp are 6 active DOF (provided of 6 actuators, by the 6 sliding motions between elements 1 and 2) and 12 passive DOF (rotations on elements 1 and 2 related to axis  $A_0B$ ). The general formula of mobility can be written, for PMp-s from

the second category (fig. 2), in the following form:  $M = \left( \sum_{m=1}^5 (m \cdot C_m) - \left( \sum_{i=1}^{n_c} r_i + r_c \right) \right) \cdot N_l + r_c$ , where:  $\sum_{m=1}^5 (m \cdot C_m)$  are

the number of a leg joints,  $r_i$  is the rank of closed kinematical contour of a leg structure,  $n_c$  is the number of closed contours of leg and  $r_c$  is the rank of closed contour including the mobile platform. For example, for PMp (fig. 2a),  $N_l=3$  legs and a leg is composed of a closed contour of spatial pentagon type (with the rank  $r_1=6$ ) and an open contour ( $r_2=6$ ), therefore  $n_c=1$ , while  $r_c=6$ . The geometrical mobility of this PMp is :  $M = [(1 \cdot 2 + 3 \cdot 4) - (6 + 6)] \cdot 3 + 6 = 12$ .

The 12 DOF of PMp are 6 active DOF (circular arrows with continuous line) and 6 passive DOF (circular arrows with dashed line). In the case of PMp from figure 2b  $N_l=3$  legs and a leg is composed of a closed contour of planar pentagon type (with the rank  $r_1=3$ ) and an open contour (with the rank  $r_2=6$ ), therefore  $n_c=1$ , while  $r_c=6$ . The geometrical mobility of this PMp (fig.2b) is:  $M = [(1 \cdot 5 + 4 \cdot 1) - (3 + 6)] \cdot 3 + 6 = 6$ . All the 6 DOF of this PMp (fig. 2b) are active DOF being represented by the rotations of 6 elements marked with 1 on kinematical scheme.

References

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2. Antonescu O., Antonescu P., *Contributions to topologic structural synthesis of the parallel manipulators*. Conference of Robotics, Iasi, 2006.