

PROPRIETES OF COATINGS NIP/SIC BY TREATMENT TO 190°C REFLECTED IN THE HARDNESS

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Abstract: The experimental data of Vickers microhardness tests performed on a NiP/SiC have been interpreted in the framework of a theoretical model that attempts to conciliate the indentation size effect (ISE effect) with the Kick law that admits the measured hardness as being independent on the load applied on the indenter.

1. INTRODUCTION

Indentation hardness is the simplest method to characterize the mechanical properties of materials. Its usefulness has been greatly enhanced by the modern possibility to apply hardness tests at microstructural and even at nanoscale level. Since the indentation hardness test is performed by applying a pressing force F on the polished surface of the specimen and by measuring the area of the impression left by a hard standardized indenter or its depth of penetration.

2. THE HAYS-KENDALL THEORETICAL MODEL FOR THE ISE EFFECT

This model attempts to conciliate the Kick law with the ISE effect.

The Kick law involves the supposition that microhardness is constant for a given substance.

The Kick law suppose a quadratic relationship between load F and size d of the indentation diagonal:

$$F = ad^2 \quad (1)$$

This type of relationship between the measurable quantities F and d is just a straight forward consequence of the definition of the indentation hardness that is obtained by dividing the load F to the area of the indentation $H = F / A$. Indeed for the Vickers diamond pyramidal indenter with an apex angle 136°, the microhardness H_V is calculated as:

$$H_V = \frac{F}{d^2 \sin \frac{136^\circ}{2}} = 1854,4 \frac{F}{d^2} = a' \frac{F}{d^2} \quad (2)$$

where H_V is expressed in kgf/mm², F is expressed in gram.force and d is expressed in micrometers. If the load F is expressed in milliNewton the numerical constant a' in eq. (2) becomes 189,1 while the hardness H_V is expressed in daN/mm².

Ecuation (2) may be rearranged:

$$F = \frac{HV}{a'} d^2 \quad (3)$$

It is obvious that if one supposes the hardness HV being constant for a given material a new constant:

$$K = \frac{1}{a'} HV \quad (4)$$

appears in eq. (3). So eq. (3) has transformed itself into eq. (2) that is just the Kick law.

Unfortunately the ISE effect invalidates the Kick law if the applied load is low. In fact at low values for the applied load F the indentation hardness appears to be dependent on F.

The problem that arises is how to conciliate the Kick law with the existence of the ISE effect, that in some experimental conditions invalidates it. A way to do this was proposed by Hays and Kendall [3] and it was mainly applied for metallic materials. In this theoretical model the Kick law is admitted to be valid in whatever conditions but the effective load F_{eff} involved in producing the plastic deformation responsible for the appearance of the indentation is less than the applied load F by a quantity W. Then the Kick law must be written as follows:

$$F - W = Kd^2 \quad (5)$$

where W represents the resistance of the material to yielding or the force required to initiate the plastic deformation in the material. Then eq. (5) may be rewritten as follows:

$$F = W + Kd^2 \quad (6)$$

3. EXPERIMENTAL RESULTS

A series of Vickers microhardness tests have been performed at various applied loads F from 15 to 300 gram force for a four material composites NiP/SiC. The size d of the indentation diagonal was taken as the average of ten measured values for each material composites NiP/SiC and each applied load F.

In the series of figures Fig. 1- 4 we have represented the dependence $F=f(d^2)$ for four material composites NiP/SiC by treatment to 190°C taken under study.

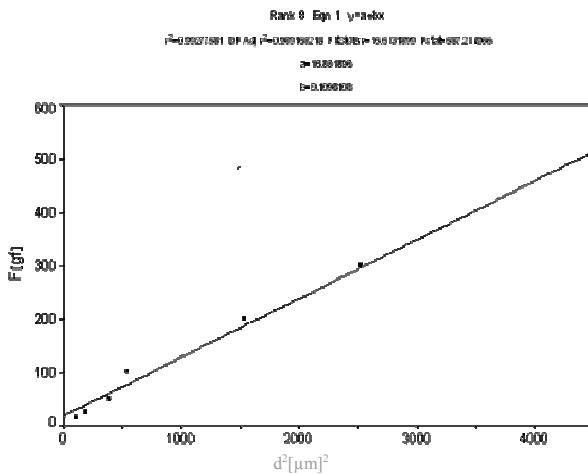


Fig.1: Quadratic plot of the experimental data recorder for $P0S40_{tt190}^0C$ (Hays-Kendall model $F = W + Kd^2$)

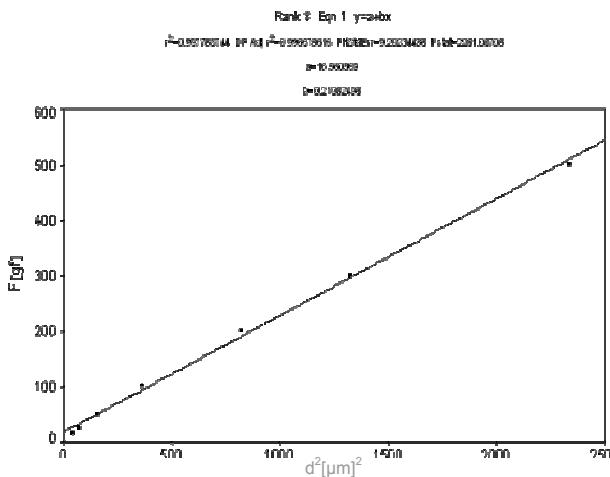


Fig.2 Quadratic plot of the experimental data recorder for a $P5S40\text{-}tt\text{-}420}^0C$ (Hays-Kendall model $F = W + Kd^2$)

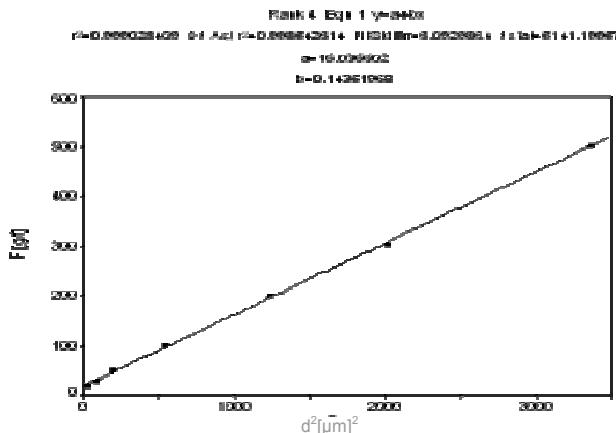


Fig.3: Quadratic plot of the experimental data recorder for a $P10S40\text{-}tt\text{-}190}^0C$ (Hays-Kendall model $F = W + Kd^2$)

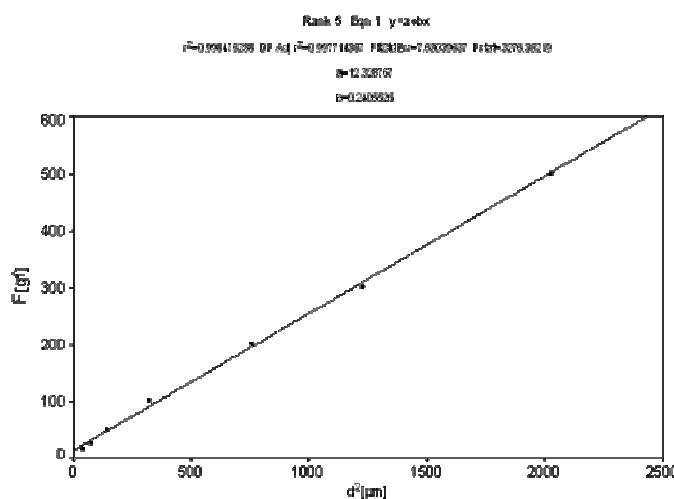


Fig. 4: Quadratic plot of the experimental data recorder for a P20S40-tt-190°C
(Hays-Kendall model $F = W + Kd^2$)

It is worthy to mention that the measured values for d^2 (the square of the verage diagonal of the Vickers indentation) were obtained at various indentation loads ($F=15; 25; 50; 100; 200; 300\text{gr.f}$). It was obtain a very good coefficient r^2 comprised between 0,992 and 0,999 for all composites NiP/SiC by treatment to 190°C.

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