

## STUDY ON A MECHANISM WITH A THREE-SLIDING TRIAD, USED TO SCISSORS

LUCA Liliana\*, POPESCU Iulian\*\*, RADULESCU Constanta\*

\*University Constantin Brancusi Targu-Jiu, \*\*University of Craiova, Romania,  
[lylyanaluca@yahoo.com](mailto:lylyanaluca@yahoo.com), [rodicaipopescu@yahoo.com](mailto:rodicaipopescu@yahoo.com)

**Keywords:** triad, press mechanism, analysis mechanism

**Abstract:** It is being studied the kinematics of a mechanism which has triad with links, one outdoor and three indoor. We adopt a range of sizes for the mechanism, we write the relations for positions and we determine the successive positions. It appears that the mechanism satisfies the conditions imposed by technology, meaning the press cuts out, on the fly, with this mechanism, a metallic or non-metallic strip of material. They are written the relations for speed and acceleration. They are determined the charts of positions, velocities and acceleration. The calculations and the charts confirm the proper functioning of the mechanism.

### 1. Introduction

They are known many mechanisms used in different types of mechanical scissors. In [1] is also indicated the mechanism of fig. 1, which has two conductive elements 1 and 1' and 2 and 3 links are solidarity with H and H' knives. We decided to study further the possibilities of this mechanism. In [2] is being studied the kinematics of a mechanism with triad, and in [3] are established the triad aspects, by kinematics.

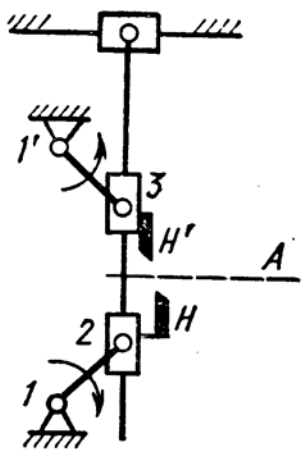


Fig. 1. Mechanism for scissors

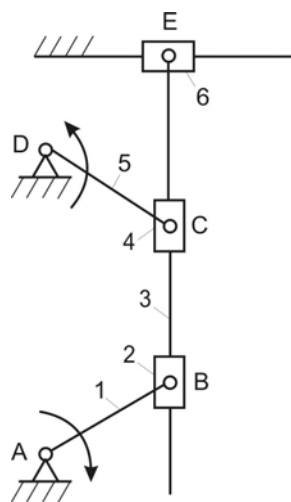


Fig. 2. Kinematic Scheme

### 2. The mechanism structure

The kinematic scheme of the mechanism, which is required for structural analysis, is given in fig. 2. The mechanism has 6 movable elements and 8 joints of fifth grade, so the degree of mobility is  $M = 2$ , the conductive elements are 1 and 5. In fig. 3 is shown the structural scheme and in fig. 4 is given the decomposition in kinematics groups. It appears that the mechanism is composed of two cranks, 1 and 5, and a triad of 3<sup>rd</sup> order, which has an outer and two inner flies, which is a rare triad.

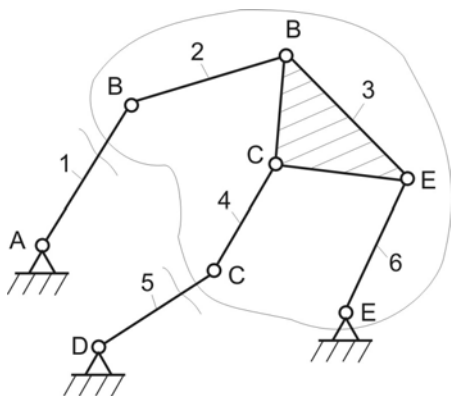


Fig. 3. The structural scheme

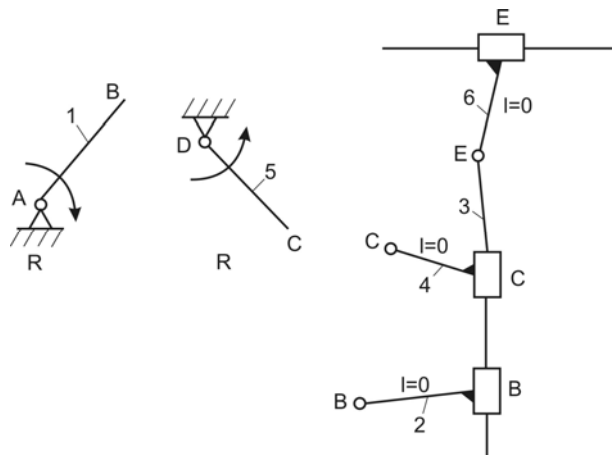


Fig. 4. R + R + Triad

### 3. The positions analysis

Based on the notations of fig. 5, are written the relations:

$$\begin{aligned}
 x_B &= a \cos \varphi ; y_B = a \sin \varphi & (1) \\
 x_C &= b \cos \psi ; y_C = y_D + b \sin \psi & (2) \\
 S_6 &= x_B = x_C ; S_2 = y_E - y_B ; S_4 = y_E - y_C ; S = S_2 - S_4 & (3)
 \end{aligned}$$

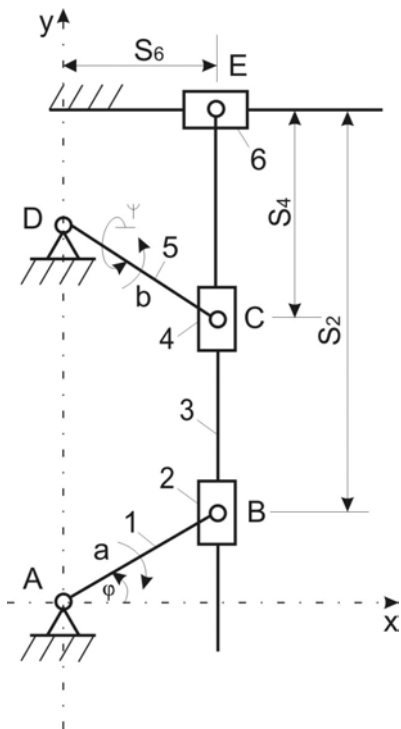


Fig. 5. The scheme for computing

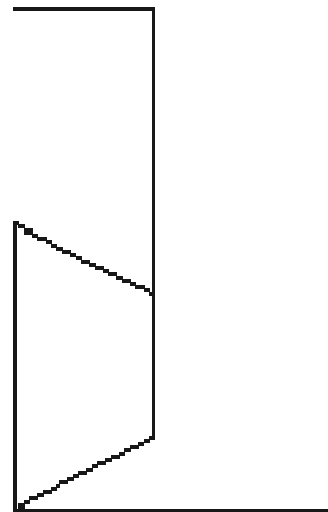
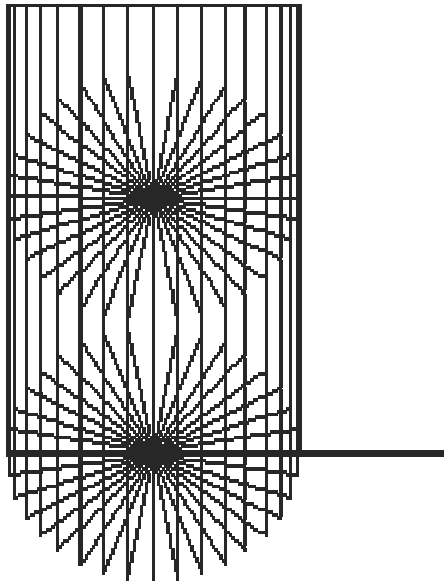


Fig. 6. The modeled position of the mechanism

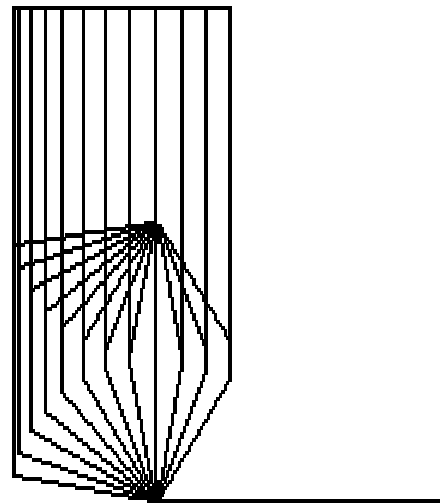
Figure 6 shows the mechanism position, shaped with these relations, similar to that of figure 5.

Were adopted as mechanism dimensions the following:  $a = b = 0.1$  m,  $0.2$  m  $y_D =$ ,  $y_E = 0.35$  m,  $n = 120$  rpm, considering the fine mechanics domain. The movements of the two cranks are connected as follows:  $\varphi = -\psi$ .

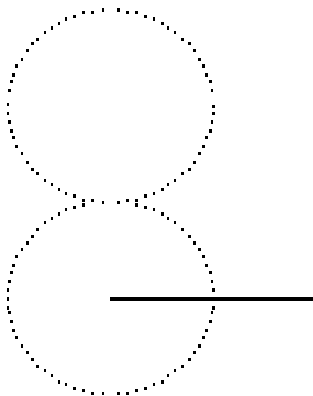
Successive positions of the mechanism are given in figure 7. Observe the symmetry positions of the cutter contact area, detailed in Fig. 8 and 9 ( $\psi = 180 \dots 330$ ).



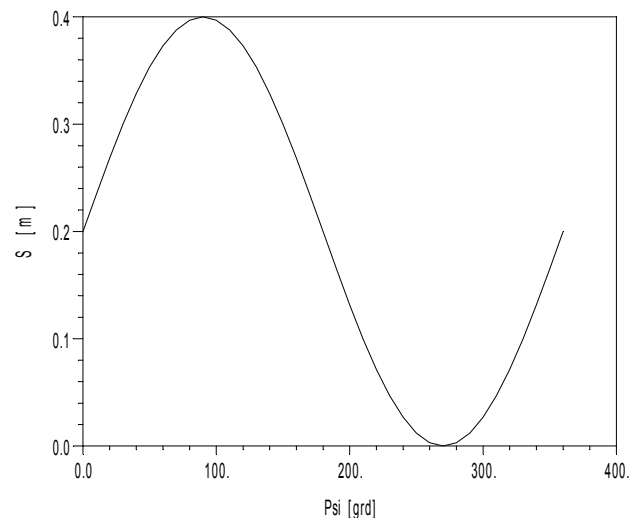
**Fig. 7. Successive positions of the mechanism**



**Fig. 8. Positions for the contact area**



**Fig. 9. The circles described by C and B**

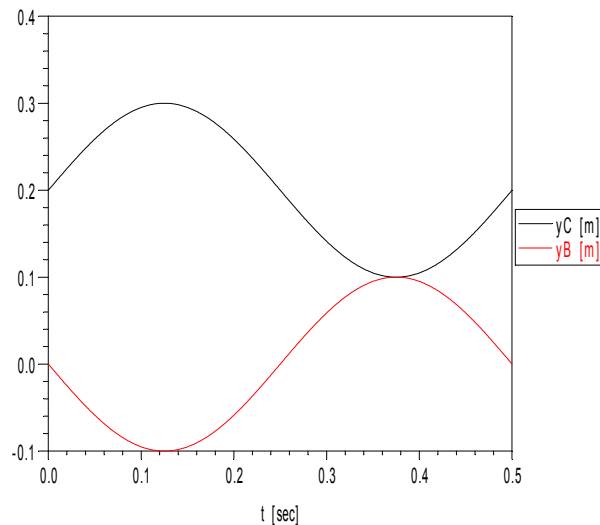


**Fig. 10.  $S(\psi)$  law**

Changes in race  $S$ , meaning in the distance between the two cutters, is given in fig. 10. From fig.1 and 10 we observe that are two links that do not touch, but peaks of  $H$  and  $H'$  cutters reach the same order, when  $\psi = 270$  degrees. Starting from  $\psi = 0$ ,  $H'$  cutter climbs,

reaching a maximum at  $\psi=90$ , then down to  $\psi=270$  and climbs back up to  $\psi=0$ . Shearing occurs when rotating cutters, just heading  $\psi=270$  degrees, moment at which useful forces are maximum.

In figure 11 we see the ordinates variation of C and B points in relation to time. Is observed as one increases and the other decreases, symmetrical, being tangent to  $\psi=270$  degrees, meaning at  $t=0.1$  seconds (Table 1). Table 1 gives these values for the interest area, ascertaining the symmetrical variation of the two ordered. It thus appears that the mechanism satisfies the imposed conditions.



**Fig. 11. Ordinates variations of C and B points**

**Table 1**

Psi	t	yC	YB
260	.3611111	.1015193	9.848072E-02
261	.3625	.1012312	9.876879E-02
262	.3638889	.1009732	9.902676E-02
263	.3652778	.1007454	9.925457E-02
264	.3666667	.1005478	9.945216E-02
265	.3680556	.1003806	9.961944E-02
266	.3694444	.1002436	9.975638E-02
267	.3708333	.1001371	9.986293E-02
268	.3722222	.1000609	9.993908E-02
269	.3736111	.1000152	9.998476E-02
270	.375	.1	.1
271	.3763889	.1000152	9.998478E-02
272	.3777778	.1000609	9.993911E-02
273	.3791667	.100137	9.986298E-02
274	.3805556	.1002436	9.975644E-02
275	.3819445	.1003805	.0996195
276	.3833333	.1005478	9.945224E-02
277	.3847222	.1007454	9.925465E-02
278	.3861111	.1009731	9.902686E-02
279	.3875	.1012311	.0987689
280	.3888889	.1015192	9.848084E-02

The  $t(\psi)$  correlation and race variations are given in fig. 12.  $S_6$  curve shows that E point (fig. 2) goes to the left, exceeds y axis, reaches a minimum at  $\psi = 180$  degrees, then returns to the right, exceeds y-axis and reach its original position.

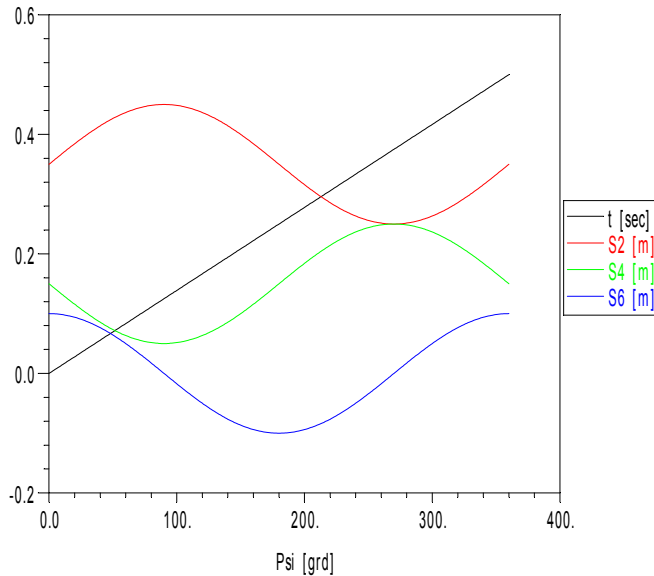


Fig. 12. Races variations

#### 4. Speeds and accelerations

It derivates twice with respect to time, the relations from positions, resulting in:

$$\dot{x}_B = -a \sin \varphi \cdot \dot{\varphi} ; \dot{y}_B = a \cos \varphi \cdot \dot{\varphi} \quad (4)$$

$$\dot{x}_C = -b \sin \psi \cdot \dot{\psi} ; \dot{y}_C = b \cos \psi \cdot \dot{\psi} \quad (5)$$

$$\dot{S}_6 = \dot{x}_B = \dot{x}_C ; \dot{S}_2 = -\dot{y}_B ; \dot{S}_4 = -\dot{y}_C ; \dot{S} = \dot{S}_2 - \dot{S}_4 \quad (6)$$

$$\ddot{x}_B = -a \cos \varphi \cdot \dot{\varphi}^2 - a \sin \varphi \cdot \ddot{\varphi} ; \ddot{y}_B = -a \sin \varphi \cdot \dot{\varphi}^2 + a \cos \varphi \cdot \ddot{\varphi} \quad (7)$$

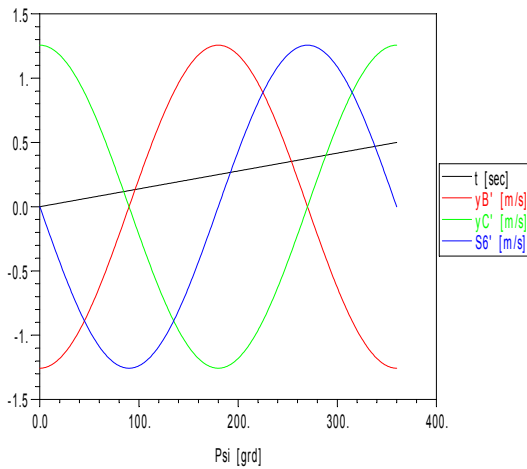
$$\ddot{x}_C = -b \cos \psi \cdot \dot{\psi}^2 - b \sin \psi \cdot \ddot{\psi} ; \ddot{y}_C = -b \sin \psi \cdot \dot{\psi}^2 + b \cos \psi \cdot \ddot{\psi} \quad (8)$$

$$\ddot{S}_6 = \ddot{x}_B = \ddot{x}_C ; \ddot{S}_2 = -\ddot{y}_B ; \ddot{S}_4 = -\ddot{y}_C ; \ddot{S} = \ddot{S}_2 - \ddot{S}_4 \quad (9)$$

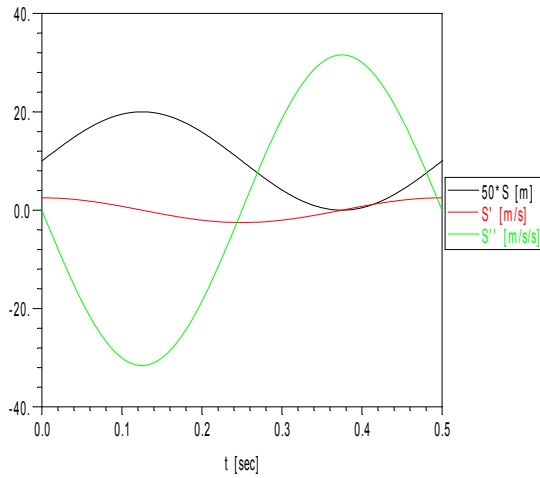
From figure 13 are observed the symmetrical variations of the points C and B vertical components velocity, with zero values at  $\psi = 90$  and  $270$  degrees, and also the variation of E speed.

In figure 14 were given the variations of S, S', S'' parameters with time t. For reasons of scale, it was represented  $50 \cdot S$ . The curves are sinusoids and cosine, so they have symmetries and thus are kinematics correlated.

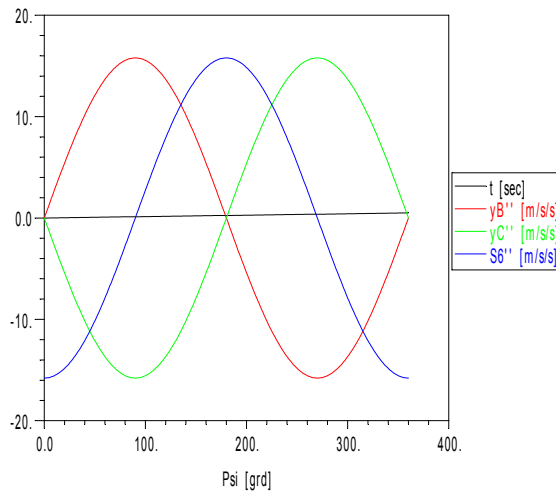
The accelerations variations are given in figure 15, the curves are all trigonometrics, with symmetries.  $y_B''$  and  $y_C''$  have opposite values at  $\psi = 90$  and  $270$  and are zero at  $\psi = 0, 180, 360$  degrees.



**Fig. 13. Velocity variations**



**Fig. 14 The variation  $S=BC$ ,  $S'$ ,  $S''$  with  $t$  time**



**Fig. 15. Acceleration variations**

## 5. Conclusions

The mechanism is intended to press that cuts out, on the fly, a metallic or non-metallic strip of material. The mechanism satisfies the imposed conditions. Charts of the positions, velocities and accelerations confirm proper functioning of the mechanism. Although it contains a triad with sliding, the mechanism calculation is easy, due to symmetries.

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